

Exact nonequilibrium work generating function for a small classical systemW. A. M. Morgado^{1,*} and D. O. Soares-Pinto^{2,†}¹*Departamento de Física, Pontifícia Universidade Católica and National Institute of Science and Technology for Complex Systems, 22452-970 Rio de Janeiro, RJ, Brazil*²*Instituto de Física de São Carlos, Universidade de São Paulo, P.O. Box 369, 13560-970 São Carlos, SP, Brazil*
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We obtain the exact nonequilibrium work generating function (NEWGF) for a small system consisting of a massive Brownian particle connected to internal and external springs. The external work is provided to the system for a finite-time interval. The Jarzynski equality, obtained in this case directly from the NEWGF, is shown to be valid for the present model, in an exact way regardless of the rate of external work.

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I. INTRODUCTION

Due to the development of precision manipulation techniques at very small length scales, such as atomic force microscopes or optical tweezers, it has become possible to study the response of small systems to applied external influences, such as the work done by pulling apart the extremities of DNA molecules [1–3]. These nonequilibrium experiments can yield equilibrium information (free energies) about the system [4,5]. This can be obtained from relations such as the Jarzynski equality [6,7] (JE). The explicit form for the JE [6] relating the external work fluctuations and the variation ΔF of the free energy between these two states is

$$\overline{\exp\{-\beta W\}} = \exp\{-\beta \Delta F\}. \quad (1)$$

In order to understand the equality above, we observe that an important step in the derivation of Fluctuation Theorems, and the JE, is to make sure that the changes in the values of the Hamiltonian of the system are directly associated with the external work performed by the environment onto the system [8,9]. In fact, the distinction between environment and system is a matter of choice. We can decide which variables are accounted for as belonging to the system, the remaining being part of the environment. In fact, conservative external forces might be incorporated into the Hamiltonian of the system as potential-energy terms [8], thus making the total Hamiltonian invariant under its effect. So, for an isolated system the external work verifies (x and p represent all phase-space variables)

$$W_{\text{external}} = \mathcal{H}(x_2, p_2, t_2) - \mathcal{H}(x_1, p_1, t_1), \quad (2)$$

where positions and momenta evolve from state 1 to state 2 according to the dynamics of the system. However, external forces arising from rheonomic constraints [10] might perform work on the system but, since they do not come from a simple expression of a conservative potential energy, they cannot be simply incorporated into the Hamiltonian as above. On the other hand, their work expression can be derived from the constraint's equations [10]. In fact, these

forces can do work on an otherwise isolated system and change the Hamiltonian energy landscape upon which the phase-space point evolve in time [11]. Thus, one has to be quite careful when defining the external work, as that choice can substantially change the final form for any fluctuation relation [9]. Indeed, fluctuation relations that are derived under distinct choices of the definition of work used will lead to distinct forms of the fluctuation theorems [8,9,12–21] (FT).

The JE have been demonstrated exactly for systems initially thermalized at temperature T , that can be either mechanically closed or in contact with a thermostat (at temperature T also) all the time. These results are obtained for systems that are large enough so that they may be placed into a true equilibrium state for which a valid partition function exists, and a correspondingly valid free energy associated with it [22], according to the usual derivation of the canonical ensemble distribution. On the other hand, given the Hamiltonian for a small system, one can define its canonical partition function and calculate the corresponding free energy.

Several models [23–31] have been proposed where the JE is verified for distinct systems. In particular, for Ref. [23], the system consists of a particle pulled through a thermal bath in a manner that becomes time invariant as $t \rightarrow \infty$. We propose the present model as a realization of a nonequilibrium process for a system that is clearly nonhomogeneous in time. Irrespective of the duration of the process, the amount of external work done is finite, in average, and fluctuates around a well defined value.

Our model consists of a Hamiltonian that incorporates the kinetic energy term of a Brownian particle, and the potential-energy terms associated with two springs connected to the particle: one represents a harmonic potential centered at $x=0$ and the other spring has one end fixed on the particle while the other end is pulled, according to a given time protocol, as work is done on the system (mass and two springs) by the external constraint force at the pulling end of the spring. This external force is the only force that can change the energy of the system. Our choice of definition for the work follows from the discussion above and seems well suited for studying the JE. This model can be thought as a prototype of a controllable heat engine that can operate in reversible or irreversible modes.

We calculated exactly the model dynamics, in the spirit of other models previously used by the authors [32,33], and we

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analyzed the behavior of external work fluctuations that are in contact with thermal bath. The thermal bath is represented by a noise term in a Langevin equation (LE) [34]. We approach that problem from the point of view of a nonequilibrium work generating function (NEWGF), equivalent to the complete nonequilibrium work probability distribution. Such functions have been used in the context of the JE [35,36]. They allow us to obtain the work probability distribution for equilibrium and nonequilibrium conditions.

Starting from the LE for an underdamped Brownian particle, we obtain exact information on the structure of the NEWGF. Solving exactly the LE for a system where the noise stochastic properties are known is akin to solving the Kramers-Moyal equation [34] for the probability distribution. Establishing exact finite-time Langevin dynamics results gives us the possibility to calibrate analytical or numerical models via the JE, in other words, it is a first principles calculation that corroborates the validity of JE, and it can also serve as a detailed testing ground for numerical simulation models. The model consists of a Brownian particle of mass m , under the action of a harmonic potential k , and in contact with a thermal reservoir at temperature T and friction coefficient γ . We attach to that particle an external spring (k'), by one extremity, and pull the other extremity at a fixed time rate (defining the work protocol). The particle-reservoir coupling is represented by a Langevin force (noise) $\eta(t)$. The external spring has the externally moving extremity at the point $x_{spring}(t)=L(t)$, as work is externally done into the system (m, k, k') without ambiguity: the work is the product of the externally varying force applied to the moving extremity of the spring k' with its displacement dL . The model and protocol we use, varying an external coordinate according to a pre-established time rate, are equivalent to others found in the literature [9].

This paper is organized as follows. In Sec. II we define the model. In Sec. III we obtain the generating function for the work probability. In Sec. IV we derive the JE, followed by our conclusions in Sec. V.

II. MODEL

So, let us define our model LE,

$$m\dot{v} = -\gamma v - kx - k'(x - L) + \eta, \quad (3)$$

$$\dot{x} = v, \quad (4)$$

$$L = L_0(1 - e^{-t/\lambda}). \quad (5)$$

The process starts ($t=0$) with the system initially at equilibrium with a reservoir (at temperature T). The initial conditions (x_0, v_0) are distributed obeying the canonical distribution at temperature T , and with $x_{spring}(t=0)=0$. Then, the external spring is moved [given $x_{spring}(t)=L(t)$] up to $t=\tau$, which may or may not be extended to infinity. The specific

form of $L(t)$ given in Eq. (5) was chosen for being easy to manipulate, but it can be readily generalized. The rate λ can be set to any value, with $\lambda \rightarrow \infty$ corresponding to the reversible work process.

By taking the Laplace transform of the Gaussian noise function's, we obtain for the second cumulant (given that the average of η is null)

$$\langle \tilde{\eta}(z_1) \tilde{\eta}(z_2) \rangle = \frac{2\gamma T}{z_1 + z_2}. \quad (6)$$

We can integrate this system exactly by techniques similar to the ones used previously [32,33,37], where the integration paths are all described therein. However, at present, we will use a direct solution technique which is different, and simpler than that in references [32,33,37].

III. GENERATING FUNCTION FOR THE EXTERNAL WORK

In the spirit of the JE we define the precursor function to the NEWGF as

$$F(u) \equiv \exp\{-iuW_\tau\} = \sum_{n=0}^{\infty} \frac{(-iu)^n}{n!} W_\tau^n, \quad (7)$$

where the average is taken over the thermal noise, which corresponds to all possible nonequilibrium paths for the Brownian particle. In order to construct the NEWGF we need to take averages, thermal (represented by $\langle f \rangle$) and over the initial conditions (represented by \bar{f}). The expression for it reads

$$\begin{aligned} \overline{\mathcal{F}(u)} &= \overline{\langle F(u) \rangle} = \sum_{n=0}^{\infty} \frac{(-iu)^n}{n!} \overline{\langle (\Delta U + \Delta W_p + \Delta W_h + \Delta W_\eta)^n \rangle} \\ &= \exp\{-iu(\Delta U + \Delta W_p)\} \sum_{n=0}^{\infty} \frac{(-iu)^n}{n!} \overline{\langle (\Delta W_h)^n \rangle} \\ &\quad \times \sum_{n=0}^{\infty} \frac{(-iu)^n}{n!} \langle (\Delta W_\eta)^n \rangle, \end{aligned}$$

where the partial terms for the external work ΔW_p , ΔW_h , and ΔW_η will be defined in the following.

The accumulated work function, that measures the total external work done on the system up to time τ , W_τ is $\{F_{\text{ext}} = -k'[x(t) - L(t)]\}$,

$$\begin{aligned} W_\tau &= \int_0^\tau F_{\text{ext}} dL = -k' \int_0^\tau dt \frac{dL}{dt} (x(t) - L(t)) \\ &= \Delta U - k' \int_0^\tau dt \frac{dL(t)}{dt} x(t), \quad (8) \end{aligned}$$

with $\Delta U = k'L^2(\tau)/2$. It is the coupling of $x(t)$ and $\frac{\partial L(t)}{\partial t}$ will give rise to the irreversible work loss.

A few thermodynamic properties for our system can be obtained directly from the equilibrium partition function

$Z = \int_{-\infty}^{\infty} \frac{dp dx}{\hbar} e^{-\beta \mathcal{H}(x,p)}$, where $\beta \mathcal{H}(x,p) = \frac{1}{2T} [L \frac{p^2}{m} + kx^2 + k'(x-L)^2]$. We find $F = \left(\frac{kk'}{k+k'}\right) \frac{L^2}{2} - T \ln\left(\frac{2\pi T}{\hbar} \sqrt{\frac{m}{k+k'}}\right)$, $S = \ln\left(\frac{2\pi T}{\hbar} \sqrt{\frac{m}{k+k'}}\right) + 1$, and $E = T + \left(\frac{kk'}{k+k'}\right) \frac{L^2}{2}$, where T corresponds to the kinetic and elastic energy contributions around equilibrium (via equipartition theorem $2 \times T/2$). The second term on the RHS is the rest energy of two springs, k and k' , of zero length, connected serially with total extension L .

Keeping T constant, the reversible work W_r and the free-energy ΔF are identical [$L(t=0)=0$],

$$W_r = \Delta F = \left(\frac{kk'}{k+k'}\right) \left(\frac{L^2}{2}\right) = \left(\frac{k}{k+k'}\right) \Delta U. \quad (9)$$

The dissipative work $W_d = W_\tau - W_r$ can be expressed as the integral of fluctuations of x around the instantaneous equilibrium position $x^{eq} = \frac{k'}{k+k'} L(t)$,

$$W_d = -k' \int_0^\tau dt \frac{dL}{dt} \left(x(t) - \frac{k'}{k+k'} L(t)\right). \quad (10)$$

We can obtain a particular solution $x_S(t)$ associated with the source term $S(t)$, via the Green's function method, explicitly as

$$x_S(t) = \int_0^t dt' \frac{2e^{-\theta(t-t')/2}}{m\sqrt{4\omega^2 - \theta^2}} \sin\left(\frac{\sqrt{4\omega^2 - \theta^2}(t-t')}{2}\right) S(t'), \quad (11)$$

where $\theta = \gamma/m$, and $\omega^2 = (k+k')/m$.

The exact solution $x(t)$ for Eqs. (3)–(5), taken in the sense that the exact form for the Langevin term $\eta(t)$ is known (due to the linearity of the problem under scrutiny) is simply the

sum of the homogeneous solution $x_h(t)$, the term $x_p(t)$ with source $L_0(1 - e^{-t/\lambda})$, and the term $x_\eta(t)$ with source $\eta(t)$: $x(t) = x_h(t) + x_p(t) + x_\eta(t)$.

We may write the total work as

$$\begin{aligned} W_\tau &= \Delta U - k' \int_0^\tau dt \frac{\partial L(t)}{\partial t} (x_h(t) + x_p(t) + x_\eta(t)) \\ &\equiv \Delta U + \Delta W_h^\tau + \Delta W_p^\tau + \Delta W_\eta^\tau. \end{aligned} \quad (12)$$

The work expressions, for ΔW_h^τ and ΔW_p^τ are given below. The detailed form of the coefficients is given in Appendix A in Eqs. (A1) and (A2),

$$\Delta W_h^\tau = C_1^\tau x_0 + C_2^\tau v_0, \quad (13)$$

$$\Delta W_\eta^\tau = -k' \int_0^\tau dt \frac{\partial L(t)}{\partial t} x_\eta(t). \quad (14)$$

Making the summation for the NEWGF,

$$\sum_{n=0}^{\infty} \frac{(-iu)^n}{n!} \overline{(\Delta W_h)^n} = \exp\left\{-u^2 \frac{\overline{C_1^{\tau 2} x_0^2} + \overline{C_2^{\tau 2} v_0^2}}{2}\right\},$$

where $\overline{x_0^2} = \frac{T}{m\omega^2}$ and $\overline{v_0^2} = \frac{T}{m}$.

The thermal contribution for the work arises from the need to compensate the dissipative coupling of the noise term with the pulling rate expressed below,

$$\Delta W_\eta^\tau = -k' \int_0^\tau dt \frac{\partial L(t)}{\partial t} x_\eta(t).$$

The contribution above is the only source of irreversibility into the system. The expression for ΔW_η^τ is then

$$\begin{aligned} \Delta W_\eta^\tau &= -\lim_{\epsilon \rightarrow 0} \int_{-\infty}^{\infty} \frac{dq_1}{2\pi} \tilde{\eta}(iq_1 + \epsilon) \left(\frac{2L_0 k'}{\lambda m}\right) \int_0^\tau dt \int_0^t dt' \frac{e^{(iq_1 + \epsilon)t' - t/\lambda - \theta(t-t')/2}}{\sqrt{4\omega^2 - \theta^2}} \sin\left(\frac{\sqrt{4\omega^2 - \theta^2}(t-t')}{2}\right) \\ &= -\lim_{\epsilon \rightarrow 0} \int_{-\infty}^{\infty} \frac{dq}{2\pi} \tilde{\eta}(iq + \epsilon) (W_{\eta 1}^\tau(iq + \epsilon) + W_{\eta 2}^\tau(iq + \epsilon) + W_{\eta 3}^\tau(iq + \epsilon) + W_{\eta 4}^\tau(iq + \epsilon)), \end{aligned} \quad (15)$$

where the detailed expressions for the $W_{\eta j}^\tau$, listed in Appendix A.

The Gaussian property of the noise function leads to the disappearing of the odd momenta of ΔW_η^τ . The even ones are given as products of $\langle \Delta W_\eta^\tau \Delta W_\eta^\tau \rangle$, that can be expressed as sums of terms of the form,

$$\begin{aligned} I_{ij} &= \lim_{\epsilon \rightarrow 0} \int_{-\infty}^{\infty} \frac{dq_1}{2\pi} \int_{-\infty}^{\infty} \frac{dq_2}{2\pi} \langle \tilde{\eta}(iq_1 + \epsilon) \tilde{\eta}(iq_2 + \epsilon) \rangle W_{\eta i}^\tau(iq_1 + \epsilon) W_{\eta j}^\tau(iq_2 + \epsilon) \\ &= \lim_{\epsilon \rightarrow 0} \int_{-\infty}^{\infty} \frac{dq_1}{2\pi} \int_{-\infty}^{\infty} \frac{dq_2}{2\pi} \frac{2\gamma T}{(iq_1 + iq_2 + 2\epsilon)} W_{\eta i}^\tau(iq_1 + \epsilon) W_{\eta j}^\tau(iq_2 + \epsilon). \end{aligned} \quad (16)$$

There are ten possible distinct pairs above but we can show that only I_{11} , I_{12} , and I_{11} give nonzero results. Thus, we have

$$\langle (\Delta W_\eta^\tau)^{2n} \rangle = \frac{(2n)!}{n!2^n} (I_{11} + 2I_{12} + I_{22})^n,$$

yielding

$$\sum_{n=0}^{\infty} \frac{(-iu)^n}{n!} \langle (\Delta W_\eta^\tau)^n \rangle = \exp \left\{ -u^2 \frac{I_{11} + 2I_{12} + I_{22}}{2} \right\}.$$

The expression for the NEWGF reads

$$\begin{aligned} \mathcal{F}(u) &= \exp \left\{ -iu(\Delta U + \Delta W_p) - u^2 \frac{C_1^{\tau^2} x_0^2 + C_2^{\tau^2} v_0^2}{2} \right. \\ &\quad \left. - u^2 \frac{I_{11} + 2I_{12} + I_{22}}{2} \right\} \\ &\equiv \exp \{-iu\mathcal{R}_1 - u^2\mathcal{R}_2\}. \end{aligned}$$

Generating functions of Gaussian shape [38–40], for quadratic time-varying potentials, have already been found in the literature. The explicit expressions for \mathcal{R}_1 and \mathcal{R}_2 can be found in Appendix A.

IV. JARZYNSKI EQUALITY

The Jarzynski equality (JE) is verified, after some tedious, but straightforward, manipulations of the terms \mathcal{R}_1 and \mathcal{R}_2 from Appendix A, for all values of τ and λ since for $u = -i/T$,

$$\begin{aligned} \mathcal{F}\left(-\frac{i}{T}\right) &= \left\langle \exp\left(-\frac{W}{T}\right) \right\rangle = \exp\left(-\frac{\mathcal{R}_1}{T} + \frac{\mathcal{R}_2}{T^2}\right) \\ &= \exp\left(-\frac{\Delta F}{T}\right), \end{aligned} \quad (17)$$

where $\Delta F = \frac{kk'}{(k+k')} L_f^2$, and $L_f = L(\tau)$. Despite the highly non trivial dependence of \mathcal{R}_1 , and \mathcal{R}_2 , on λ and τ , at $u = -i/T$ the correct cancellations occur and the JE is verified.

We notice that by fixing the final position of the external spring $0 < L_f \leq L_0$ the ratio τ/λ gets fixed,

$$\frac{\tau}{\lambda} = \ln\left(\frac{L_0}{L_0 - L_f}\right),$$

which gives us an infinite number of distinct protocols for taking the system from state $A \equiv (L=0)$ to state $B \equiv (L=L_f)$, verifying the JE for all cases for a fixed $\frac{\Delta F}{T} = \frac{F_B - F_A}{T}$.

The Gaussian form of $\mathcal{F}(u)$ is the expected one due to the linear form of the harmonic potential [41]. The present model is an explicit dynamic solution that could be extended to other forms of the noise, in the case that its cumulants are known. In fact, for the quasistatic case, $\lambda, \tau \rightarrow \infty$ (τ/λ fixed), $\mathcal{F}(u) \rightarrow \exp\{-iu\Delta F\} \rightarrow p(W) = \delta(W - \Delta F)$. In this case, there is only one way of carrying out the process.

We can also obtain the forward ratio for the work distributions. We notice that W is finite (with probability equals to 1) and positive. The probability distribution for the total work $p(W)$ is the inverse Fourier transform of $F_W(u)$,

$$p(W) = \int_{-\infty}^{\infty} \frac{du}{2\pi} \mathcal{F}(u) e^{iuW}. \quad (18)$$

The expression for $p(W)$ explicitly reads

$$p(W) = \sqrt{\frac{\pi}{\mathcal{R}_2}} \exp\left\{-\frac{(W - \mathcal{R}_1)^2}{4\mathcal{R}_2}\right\}. \quad (19)$$

It can be seen that the average work done externally on the system is given \mathcal{R}_1 , while the variance is given by $2\mathcal{R}_2$, which is proportional to T for all λ and τ .

The ratio $p(W)/p(-W)$, not to be mistaken with the Crooks Fluctuation expression [7], can be obtained explicitly

$$\frac{p(W)}{p(-W)} = \exp\left\{\frac{W\mathcal{R}_1}{4\mathcal{R}_2^2}\right\}. \quad (20)$$

The expression above is well behaved in the instantaneous work case, $\lambda \rightarrow 0$, since averaging over an ensemble of initial conditions distributed with temperature T converges, while it becomes proportional to a delta-function when $\lambda \rightarrow \infty$, since $\mathcal{R}_2 \rightarrow 0$ in this case. In fact, the averages of the work do depend on the work rate λ and the elapsed time τ , but the JE arises regardless of it.

V. CONCLUSIONS

In conclusion, we develop an exact technique appropriate for treating a system consisting of a massive particle coupled to two harmonic springs in contact with an external thermal reservoir, represented by a Langevin force term. External work can be done by pulling one of the springs at a given rate, which is the protocol we follow. The main advantage of this model is that we can explicitly make all the calculations with no approximations. No approximations are needed in respect to the mass of the particle, the calculations being able to take care of the particle's inertia exactly. This model can be thought as a controllable, and simple, heat engine.

To the best of our knowledge, for the first a Langevin model was exactly integrated, taking into account inertia and general initial conditions, for a Brownian particle under the action of a given protocol. An exact form for the nonequilibrium work generating function (NEWGF) is obtained. The Jarzynski equality is then explicitly verified, such as predicted [6], showing that the method used in this paper can be seen as a first principle exact, and nontrivial, verification of the JE. This shows the appropriateness of using white Gaussian noise to represent the interaction between a thermal bath and a system. Furthermore, the work probability distribution is derived explicitly for this case and shows that the moments of the work W are complex functions of the work rate λ and the time interval τ .

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APPENDIX A: FINITE-TIME COEFFICIENTS

The exact finite-time coefficients are listed below.

$$C_1^\tau = -\frac{k'L_0(2\lambda\omega^2 - \theta^2\lambda - \theta)}{\sqrt{4\omega^2 - \theta^2}(1 + \theta\lambda + \lambda^2\omega^2)} e^{-\pi(2+\theta\lambda)/2\lambda} \sin\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) + \frac{k'L_0(1 + \theta\lambda)}{(1 + \theta\lambda + \lambda^2\omega^2)} e^{-\pi(2+\theta\lambda)/2\lambda} \cos\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) - \frac{k'L_0(1 + \theta\lambda)}{1 + \theta\lambda + \lambda^2\omega^2} \quad (\text{A1})$$

$$C_2^\tau = \frac{k'L_0(2 + \theta\lambda)}{(1 + \theta\lambda + \lambda^2\omega^2)\sqrt{4\omega^2 - \theta^2}} e^{-\pi(2+\theta\lambda)/2\lambda} \sin\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) + \frac{k'L_0\lambda}{(1 + \theta\lambda + \lambda^2\omega^2)} e^{-\pi(2+\theta\lambda)/2\lambda} \cos\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) - \frac{k'\lambda L_0}{1 + \theta\lambda + \lambda^2\omega^2} \quad (\text{A2})$$

$$\begin{aligned} \Delta W_p^\tau = & -\frac{\theta k'^2 L_0^2 (3\omega^2\lambda^2 - \theta^2\lambda^2 + 1)}{m\omega^2\sqrt{4\omega^2 - \theta^2}[(1 + \lambda^2\omega^2)^2 - \theta^2\lambda^2]} e^{-\pi(2+\theta\lambda)/2\lambda} \sin\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) \\ & - \frac{k'^2 L_0^2 (-\theta^2\lambda^2 + \omega^2\lambda^2 + 1)}{m\omega^2[(1 + \lambda^2\omega^2)^2 - \theta^2\lambda^2]} e^{-\pi(2+\theta\lambda)/2\lambda} \cos\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) - \frac{k'^2 L_0^2 (-2\omega^2\lambda^2 + \omega^2\lambda^2 e^{\pi\lambda} - 2\theta\lambda - 2)}{2m\omega^2(1 + \theta\lambda + \omega^2\lambda^2)} e^{-\pi\lambda} \\ & - \frac{k'^2 L_0^2 \lambda^2}{2m(1 - \theta\lambda + \omega^2\lambda^2)} e^{-2\pi\lambda} \end{aligned} \quad (\text{A3})$$

$$W_{\eta_1}^\tau(s) = \frac{k'L_0}{m(\theta s + s^2 + \omega^2)(s\lambda - 1)} e^{\pi(s\lambda - 1)/\lambda}, \quad (\text{A4})$$

$$W_{\eta_2}^\tau(s) = -\frac{k'L_0\lambda^2}{m(s\lambda - 1)(\theta\lambda + 1 + \omega^2\lambda^2)}, \quad (\text{A5})$$

$$W_{\eta_3}^\tau(s) = -\frac{(-\theta\lambda s - \theta^2\lambda + 2\lambda\omega^2 - 2s - \theta)k'L_0}{m\sqrt{4\omega^2 - \theta^2}(\theta s + s^2 + \omega^2)(\theta\lambda + 1 + \omega^2\lambda^2)} e^{-\pi(2+\theta\lambda)/2\lambda} \sin\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right), \quad (\text{A6})$$

$$W_{\eta_4}^\tau(s) = \frac{(s\lambda + \theta\lambda + 1)k'L_0}{m(\theta s + s^2 + \omega^2)(\theta\lambda + 1 + \omega^2\lambda^2)} e^{-\pi(2+\theta\lambda)/2\lambda} \cos\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right), \quad (\text{A7})$$

$$\begin{aligned} I_{11} = & \frac{\gamma T L_0^2 k'^2 (-\theta\lambda - 1 + \lambda\omega)(1 + \theta\lambda + \lambda\omega)}{m^2\omega^2\sqrt{4\omega^2 - \theta^2}(1 + \theta\lambda + \omega^2\lambda^2)^2} e^{-\pi(2+\theta\lambda)/\lambda} \sin(\tau\sqrt{4\omega^2 - \theta^2}) \\ & - \frac{\gamma T L_0^2 k'^2 (-\theta^3\lambda^2 - \theta - 2\theta^2\lambda + 4\lambda\omega^2 + 3\theta\lambda^2\omega^2)}{m^2\omega^2(4\omega^2 - \theta^2)(1 + \theta\lambda + \omega^2\lambda^2)^2} e^{-\pi(2+\theta\lambda)/\lambda} \cos(\tau\sqrt{4\omega^2 - \theta^2}) \\ & - \frac{\gamma T L_0^2 k'^2 (\theta^3\lambda - 4\theta\lambda\omega^2 - 4\omega^2 + 4e^{-\tau\theta}\omega^2 + \theta^2)}{m^2\omega^2\theta(4\omega^2 - \theta^2)(1 + \theta\lambda + \omega^2\lambda^2)} e^{-2\pi\lambda} \end{aligned} \quad (\text{A8})$$

$$\begin{aligned} I_{12} = & \frac{2\gamma T L_0^2 k'^2 \lambda^2 (\theta^2\lambda^2 - 2\omega^2\lambda^2 - 2)}{m^2\sqrt{4\omega^2 - \theta^2}(1 + \theta\lambda + \omega^2\lambda^2)[(1 + \lambda^2\omega^2)^2 - \theta^2\lambda^2]} e^{-\pi(2+\theta\lambda)/2\lambda} \sin\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) \\ & + \frac{2\gamma T L_0^2 k'^2 \lambda^4 \theta}{m^2[(1 + \lambda^2\omega^2)^2 - \theta^2\lambda^2]} e^{-\pi(2+\theta\lambda)/2\lambda} \cos\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) - \frac{\gamma T L_0^2 k'^2 \lambda^3}{m^2[(1 + \lambda^2\omega^2)^2 - \theta^2\lambda^2]} e^{-2\pi\lambda} \end{aligned} \quad (\text{A9})$$

$$I_{22} = \frac{\gamma T L_0^2 k'^2 \lambda^3}{(1 + \theta\lambda + \omega^2\lambda^2)^2 m^2}, \quad (\text{A10})$$

$$\begin{aligned}
\mathcal{R}_1 = & -\frac{k'^2 L_0^2 (1 + \omega^2 \lambda^2 - \lambda^2 \theta^2)}{m \omega^2 [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]} e^{-\tau(2+\theta\lambda)/2\lambda} \cos\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) \\
& - \frac{k'^2 L_0^2 \theta (1 - \lambda^2 \theta^2 + 3\omega^2 \lambda^2)}{m \omega^2 \sqrt{4\omega^2 - \theta^2} [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]} e^{-\tau(2+\theta\lambda)/2\lambda} \sin\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) \\
& - \frac{L_0^2 k' \omega^2 [k' \lambda^2 (1 + \theta\lambda) + m(-2 + \theta^2 \lambda^2 - 2\lambda^2 \omega^2 - \lambda^4 \omega^4)]}{2m \omega^2 [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]} e^{-2\tau\lambda} \\
& - \frac{L_0^2 k' [-k'^2 + k' \lambda^2 (\theta^2 - \lambda^2 \omega^4) + \omega^2 (m - m\theta^2 \lambda^2 + 2m\lambda^2 \omega^2 + \lambda^4 \omega^4)]}{m \omega^2 [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]} e^{-\tau\lambda} \\
& + \frac{L_0^2 k' \omega^2 (1 - \theta\lambda + \lambda^2 \omega^2) (m + m\theta\lambda - k\lambda^2 + m\lambda^2 \omega^2)}{2m \omega^2 [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]}. \tag{A11}
\end{aligned}$$

$$\begin{aligned}
\mathcal{R}_2 = & -\frac{(1 + \omega^2 \lambda^2 - \lambda^2 \theta^2) T L_0^2 k'^2}{m \omega^2 [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]} e^{-\tau(2+\theta\lambda)/2\lambda} \cos\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) \\
& - \frac{\theta T L_0^2 k'^2 (1 - \lambda^2 \theta^2 + 3\omega^2 \lambda^2)}{m \omega^2 \sqrt{4\omega^2 - \theta^2} [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]} e^{-\tau(2+\theta\lambda)/2\lambda} \sin\left(\frac{\tau\sqrt{4\omega^2 - \theta^2}}{2}\right) + \frac{T k'^2 L_0^2 (1 + \omega^2 \lambda^2 - \theta\omega^2 \lambda^3 - \theta^2 \lambda^2)}{2m \omega^2 [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]} e^{-2\tau\lambda} \\
& + \frac{T k'^2 L_0^2 (1 + \theta\lambda^3 \omega^2 + \omega^2 \lambda^2 - \lambda^2 \theta^2)}{2m \omega^2 [(1 + \omega^2 \lambda^2)^2 - \theta^2 \lambda^2]}. \tag{A12}
\end{aligned}$$

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- [11] An example of such a potential is that of an instantaneously switched-on constant force $f(t)$ [16]: for $t < 0$, there is no potential energy, while for $t > 0$ a potential energy $-f_0 x$ arises [8]. For instance, this can be thought as the energy of a very small bare electric charge placed in the inside of charged capacitor plates, with plates orthogonal to the x axis. The charging of the capacitors happens almost instantly at $t=0$, and we assume that the plates were grounded at $t < 0$. In fact, the external work done by the force, described by the equation above, corresponds to the work done by the batteries in order to initially charge the capacitors up to a fixed voltage (part of that work shifts the particles potential energy and the remaining is used to create the electric field between the plates), producing a constant force upon the particle. It has the effect of shifting the initial potential energy of the charged particle by an amount $-f_0 x_0$, where x_0 is the initial position of the charged particle (if we include the batteries within the system, then the potential energy they provide is taken to be internal). That external work is then given by consistent with references [8,9]. The important point to be consistent with is that the external work is the one changing the energy landscape for the phase-space point. In contrast, if we keep the batteries as an external agent for all t , then the total external work is given by $\phi(x, t) = -f(t)x \equiv -f_0 \Theta(t)x$. $W_{\text{ext},0} = -f_0 x_0 = -\int_{t_1 < 0}^{t_2 > 0} dt f_0 \dot{\Theta}(t)x_t$, $W_{\text{ext}} = -f_0(x_{t_2} - x_0) + W_{\text{ext},0} = -f_0 x_{t_2}$. The definition of what is the internal Hamiltonian, and what is external, is crucial as to which Work Fluctuation relation can be derived [8,9].
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